

Role Of Control Algorithms And Modeling Of System Dynamics Accuracy In Trajectory Planning Tracking For Autonomous Movement Of Robots

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Abstract:

Autonomous robots have been employed for a variety of tasks, including transporting materials among workplaces. They're also seen in a variety of settings, including industrial, healthcare, ecological, and even household equipment. As they are widely employed in a variety of industries, study on autonomous robots has increased and received a lot of interest in recent times. We present a unified regional path monitoring and scheduling strategy for automated ground robotics (AGRs) movement across a standard path including static barrier rejection in this study. We split the pathway leading work into two sub-works rather than using typical crossing track-based feedback devices to direct the robot as accurately as appropriate to a standard pathway. To begin, we use effective design-based forecasting path planning to pursue the standard route with seamless movements while also avoiding barriers. This planning perceives sculptural data of the designated route, motion restrictions, and partialdynamic restrictions to acquire a collision-free as well as the dynamically-feasible pathway in every planning process. The path is being supplied to the low-level path monitoring controllers. We create an interior modeling controller based on robotics steady-state driving features to monitor the desired path while avoiding the adverse impacts of modeling uncertainty and exterior disruptions. The suggested methodology can seamlessly implement a standard trajectory while ignoring fixed barriers at a great velocity, as demonstrated by the outcomes. To enhance the path tracking speed, even more, an enhanced incremental learning control strategy is being used to repress the impact of the original state inaccuracy while using less processing period. The suggested control approach is successful and practicable for path planning management of mobile robots, particularly when a high level of actual time is required, as demonstrated by experimental findings.

Keywords: Iterative learning method, Control Mechanism, Automated Ground Robots (AGRs), Path tracking.

INTRODUCTION

The domain of automated navigation has seen fast progress over the last three decades, attracting significant research attention and initiatives from both academics and businesses. Operator assistant

technologies have already implemented partly automated control tasks, and various automobile corporations are developing study and improvement predictions for future automated robots. However, there are still a lot of obstacles to overcome to produce truly dependable and durable completely automated robots that can manage a variety of realistic circumstances in actual life. The creation and use of AGVs, which are very well known, necessitates the combination of state-of-the-art techniques spanning from vision, positioning to guidance and management [1]. Both regional motion planners and the route planning controller, as key components, play an important role in ensuring security and enhancing robots' performance.

Many scientists created Lyapunov-based feedback controlling legislation by analyzing robotic kinematics and dynamics, like slider modeling controls, backstepping controls, etc, to monitor the standard path precisely and reliably. Several types of research investigate cascaded or multi-tiered control systems, concentrating on decreasing transverse faults in outer loops and stabilizing yaw movements through guiding movements in the inner loop, to accommodate high velocity and varied terrain circumstances and increase control precision and resilience [2]. Tire sideslip inclinations and inertia factors are used to eliminate modeling imperfections and exterior disruptions. When robots depart far from a standard pathway or make a tight bend, it can simply result in rapid steering maneuvers. Gain-scheduling or dynamic structural control techniques are used by certain researchers to prevent rapid control strategies and provide smooth movements at the sacrifice of monitoring precision or error convergence rate [3].

Depending upon an analysis of a variety of pathway monitoring controllers, [4] determined that pathway monitoring control efficiency is substantially influenced by both robotic kinematics and the regularity of the standard path. Some of such mechanics-based and/or dynamics-based controllers were designed to eliminate present cross-track faults rather than using predicted data to completely improve a series of control methods and their associated course that effectively governs the robot's transition from its existing condition to sampled states that are matched with a standard path forward. Using optimization methods, there exists a lot of research in combined scheduling and controlling systems for AGVs. Model Prediction Control (MPC) represents one of the best appealing strategies because it can convert the robots' navigation issue into the finite-horizon restricted optimization controlling issue [5]-[7]. The MPC method employs the robots' kinematic or dynamic models to forecast future condition progression depending upon present measurements. It produces a series of control methods in every controlling cycle that minimizes a given objective function within such a limited horizon while also satisfying the management restrictions.

At the moment, there will be two basic approaches to analyzing and designing a robot manipulator path monitoring controller [8]. First is a comparison with such a traditional linear control approach [9, 10]. This approach is simple, as well as some traditional control theories and methodologies can be immediately applied to certain nonlinear features that are either estimated into such a linear relation else ignored. Furthermore, path monitoring management of robot manipulators is a multi-input as well as multi-output (MIMO) controlling issue, as well as a mobile robot with numerous dimensions of freedom has highly linked and complicated motion equations [11]. If every point is intended to be autonomous and has the same inertia, this can lead to inconsistencies in overall damping as well as

other unanticipated occurrences throughout the workplace [12]. As a result, there seems to be a second approach [13–15], which concentrates mostly on a nonlinear controlling scheme without the previous constraints. Unfortunately, such a nonlinear approach has several limitations; for instance, when designing the manipulator, it must have proper data structures and accurate parameters to accurately capture each of these difficulties, such as the communication among robotic limbs as well as the variation in centroid.

The path monitoring speed is greatly influenced by the beginning state inaccuracy. To quickly reduce the effect of the beginning state inaccuracy, an incremental learning control mechanism is applied. The path monitoring performance can be improved by using acceptable learning gain matrices. Several studies have been conducted to acquire the best learning gains, such as the dynamic exponential gain approach [16], the fuzzy PID technique [17], as well as the technique integrating neural network controllers and compensating controllers [18]. The sophisticated control rule and learning rule, on the other hand, will add a significant amount of computing time and slow down the path monitoring performance. As per the preceding study, both the conventional linear controlling approach and the nonlinear controlling approach have their own set of benefits and drawbacks. Not only can the research and development of path monitoring control be made simpler, but the efficiency and precision of path monitoring control can also be increased if the advantages of the traditional linear as well as nonlinear controlling techniques can be combined.

LITERATURE REVIEW

Many well-known sample-based motion control algorithms have been widely investigated to resolve the local path generating issue. The majority of them use a discontinuous optimization strategy. Based on the systemic model, a collection of path possibilities is developed using advanced simulations. Then, using a fitness function, the optimal path is chosen. The control space sample-based approach and condition space sample-based approach are the two types of sample-based motion scheduling schemes [19]. The former system utilizes statistical forward cooperation of differential calculus that governs robotic kinematics or dynamics to create a collection of path aspirants by discretizing the monitoring input space (like constant-curvature arcs [20], clothoid [21], or iterators of such brief movements [22]). As a result, the derived path possibilities are movable by necessity. The approach has been extensively used for regional guidance according to its ease and computing speed and is particularly appropriate for determining a collision-free pathway in less restricted environments.

Many scientists construct a motion basic library offline on body-centered coordinates and utilize these online through proportion and translations depending upon on symmetric structure of mechanical devices [23]. Despite this, the movement primitives are frequently not well-separated because they are formed by extracting the controlled input space. The comprehensive collision-testing and analysis approach will demand a significant amount of computer resources. A state-space sample-based movement planning technique, on the other hand, rather than sampling continuous control inputs, samples a collection of terminating states employing navigation pathways and surrounding information. Several approaches have been proposed to generate trajectories, which connect the robot's current state with the terminal states aligned with the reference path. It takes into consideration, not just the

location restrictions, as well as the standard path's direction and curvature aspect restrictions. A collection of terminating states is evaluated lateral offset along the standard pathway to match with standard path and get a collision-free as well as generally smoother path.

To construct continuous-curvature routes with an upper-bound curving limit [24] proposed an effective and logical pathway smoothing technique, depending upon cubic Bézier curves. [25] proposed a geometrical approach to creating various path choices using the standard pathway as a basis. The basis must be regular enough to assure that the produced alternatives are smooth. Instead of employing geometric approaches, [26] and [27] offered local interactively viable path planners that included closed-loop controlling legislation (kinematic-based nonlinear control rule and purely pursuing control rule, correspondingly) and systems, condition, and control restrictions, irrespective of the basis regularity. [28] proposed a modeled predictive path generating technique that reduces the local path generation issue to such a two-point boundary values problem (BVP) with high-fidelity robotic dynamical restrictions.

It reaches a great level of effectiveness and flexibility due to such employment of the quantitative resolving approach. For monitoring control, the low-level processor uses an open-loop control method. Fateh and Arab [29] have devised a novel voltage control scheme focused on a resilient control method. The robot kinematics, as well as state-space modeling of electric voltage, are combined to provide a comprehensive controlling framework for operating a non-holonomic WMR in this paper. In some other advancements, the actively forces control (AFC) technique has been widely used to regulate the kinematics of a robotic manipulator system, resulting in a reliable control strategy, particularly when disruptions are present [30-33]. To calculate the feedback signals of the control scheme, the approach relies on observations of delivered torque and velocity, as well as a good estimation of the predicted inertial matrix [34–36]. For route monitoring control of such a robotic manipulator, a calculated torque controller is paired with a unique modeling state observer's control [37].

The model-assisted expanded state observers were also employed to minimize structured/unstructured sounds and improve calculated friction control efficiency to obtain an accurate dynamical model and reduce the impact of sounds. The observers can evaluate the ambiguities in the complex system and adjust for disruptions online, resulting in a stable robotic manipulator path monitoring control with strong disruption rejecting capabilities. The WMR manipulator within task space gets controlled by another path monitoring robotic system that uses a computational torque control approach with dynamical models [38]. It has been demonstrated that the system's reliability is ensured and also that monitoring faults have converged employing a well-known concept of computational torque controlling.

Controlling the mobile robot in such a highly complicated context, including a highway roundabout setup while pathway implementation is still considered a difficult topic in mobile robot study because monitoring errors must be kept to a minimum [39]. As a result, a reliable controller is required to ensure minimal monitoring errors throughout the motion. AFC (activity force control) has also been extensively utilized for managing the robot's complexities and rejects disruptions, although it tending to overshoot monitoring errors also at the start of motion when the trajectory changes abruptly.

Figure 1 depicts a basic system design for an automated robot. The ambient information around the robot, as well as the robot location and posture, are provided by the detection and positioning system collected via onboard sensors. The assigned task determines the high-level operation strategy. While the mobility designers reason regarding pathway conditions, traffic rules, and other restrictions, the behavioral planners offer secure and practical actions. However, reference pathway modeling and motion analysis, which mainly concentrate on creating a collision-free route or trajectories in keeping with high-level goals, are commonly found at the mobility planning stage. The low-level monitoring controller relates to precisely monitoring the resulting trajectories.



Figure 1: Basic design of the automated robot.

TRAJECTORY PLANNING

A. TERMINAL STATES SAMPLING BASED ON A REFERENCE PATH

The automated robot's navigation must be lined with a pathway lane instead of conserving time and energy, according to the observation of robots' behavior. Because of all this, we adopt the curvilinear coordinate structure, which relies on the standard route to represent the referencing path, rather than the exact inertial coordinate's structure. We examine termination states that are coordinated with path geometry to fulfill the restrictions given by it. Furthermore, the bias-sampling approach minimizes computational expense while also preventing the robot from reaching potentially unsafe situations. We utilize a four-dimensional state description, which includes location (x, y), direction, and curve, to minimize sudden guiding actions and assure curvature-continuity of a resulting path. The terminating states must be evaluated in such a high-resolution state vector to get a collision-free as well as seamless path. Furthermore, because of restricted onboard processing resources, sample intensity and range must be reduced. As a result, as seen in Figure 2, we use an effective low-alternation sampling technique. As in the longitudinal axis, a minimum look-ahead range is frequently specified as a factor of

the robot's exact velocity to assure the minimum collision distance and overcomes the lag caused by actuators and robot inertial impacts to assure control consistency. We also establish lateral offset boundaries. The sample density and length can be changed to suit the situation as well as the accessible processing capabilities.



Figure 2: Low-alternation sampling technique.

B. MODEL PREDICTIVE PATH GENERATION

High dynamical modeling may be used to accurately anticipate the robot's evolutionary states. Moreover, because it relates to a variety of time-varying properties, it is necessary to use online recognition techniques to properly predict these values in actual time. Nonetheless, the parameter fluctuations generated by the tire-ground contact are hard to forecast. However, we use robotic kinematic modeling to forecast the system's possible future development. To increase the reliability of the forecast, dynamical effects including such sideslip inclinations and actuator movements could be taken into consideration.

$$\dot{x}(t) = v\cos(t), \\ \dot{y}(t) = v\sin(t), \\ \dot{\theta}(t) = v\kappa, \\ \kappa = u(t)$$
(1)

Trajectories can be specified as a vector value variable of period t, as seen. A path, on the other hand, binds the geographical path as well as velocity together. The path is subjected to rigorous velocity limitations. Indeed, we can follow a geometrical path without having to define velocity rules. The phases can be expressed as a factor of an arc-length s rather than time t by integrates time.

$$x(s) = \int_0^{s_f} \cos(\theta(s)) \, ds, y(s) = \int_0^{s_f} \sin(\theta(s)) \, ds$$
$$\theta(s) = \int_0^{s_f} \kappa(s) \, ds, \kappa(s) = u(s)$$
(2)

The path modeling could be broken down into geometrical trajectory planning as well as longitudinal velocities modeling in this fashion. The robotic design is changed from a time-dependent to such a spatial-dependent paradigm, allowing velocity to stay undetermined. As a result, we divide the path

creation process into two parts: The creation of geometrical paths and the scheduling of velocity. Calculating a geometrical path that fulfills the actual and tested destination states' border restrictions, the divergence restrictions are given by (2), as well as other conditions and controller input restrictions are required to solve the path generating issue. It is difficult to handle the nonlinear constraint issue utilizing nonlinear programmed techniques in the constantly controlled space due to the nonlinear divergent equations. We use the approach to initialize the controller input space then construct the path generating issue as a two-point boundary value problem (BVP) in addition to making the significant inversion issue achievable. We use a cubic polynomial spiraling framework to initialize the controller input space, it keeps the ability to articulate complicated movements and restricts independent variables. As a result, the pathways formed will also be cubic polynomial spirals.

$$\kappa(s) = \kappa_0 + \kappa_1 s + \kappa_2 s^2 + \kappa_3 s^3 \tag{3}$$

The BVP is then turned into a solution for the undetermined controller parameters $P = [\kappa_1, \kappa_2, \kappa_3, s_f]^T$.

To analyze the given BVP, we use Newton's approach presented, a relatively effective computational nonlinear optimization methodology. Newton's approach is used to repeatedly analyze the controller parameters vector P, as shown in (4). The recursive method for every BVP continues until the terminating state defects $\Delta X_F(P)$ are fewer than like a user-specified limit. The converging speed is affected by the starting estimate of parameter P. We employ a 1 pre-determined lookup-table of early values estimate by sample sparsely as in high-resolution search space to generate a suitable early estimate for online application as well as decrease the number of repeats.

$$\Delta X(P(k)) = X_{FS} - X_F(P(k))$$

$$\frac{\partial \Delta X(P)}{\partial P}\Big|_{P(k)} \Delta P = (\Delta X(P(k)))$$

$$P(k+1) = P(k) + \Delta P$$
(4)

Small fluctuations are used to compute a matrix of such a vector-valued function's first-order approximate derivatives. We evaluate lateral accelerating restrictions (as indicated in (5)) depending mostly on present speed and trajectory conditions (like pathway coefficient of friction) during the path formation stage to relieve tire sideslip impacts and minimize controller efforts for horizontal movement stabilized control. We effectively restrict wheel slip inclinations and prohibit the pressure of robotic wheels from approaching the nonlinear saturating region in this manner. Furthermore, it has the potential to greatly increase robotic stability and provide safer and higher agreeable paths, however at the cost of a reduction in state space.

$$|u(s)| \le \kappa_{max}, \kappa_{max} = f(v, \mu) \tag{5}$$

Control limitations may be simply managed because the mathematical integrating technique is used for the advanced modeling of a system. Many of the derived path alternatives are geometrically viable because the robotic kinematic modeling is expressly taken into account. We note, however, that the model predicted path planner does have limitations. This is not necessarily possible to get a collisionfree and practical resolution due to limited sample terminating stages and the limiting expression of a singular cubic spiral. A more complicated path is developed being generating strategy depending upon the spatiotemporal matrix to cope with much more difficult cases while sacrificing processing performance. The emergence control-space sample technique or sophisticated graph-search pathway design technique will be invoked if the preceding strategy fails to develop any viable and collision-free pathways.

a. Collision Check and Evaluation

We build a stated fitness function for the optimization problem to find the optimal pathway among path options. To begin, the impact check trims the pathways that collide with obstructions. Because the form of a robot is frequently rectangle, it cannot be reduced as just a mass-point. We are referring to a practical approach is described. Many circles are employed to estimate the surround of the robotic form, as seen in Figure 3. The space among the barriers and the centroid of such circles must be greater than the circumference to enable collision prevention.



Figure 3: Robot circle decomposition.

After that, a user-specified goal function is used to assess the leftover collision-free path alternatives. The impediment distance J_0 , divergence from the standard path J_d , previewing proximity J_p , smoothness J_s , and eventual consistent J_c seem to be the five weighting cost factors in this fitness function. Every cost phrase has a weighted component, which is represented by the letters $\omega_0, \omega_d, \omega_s, \omega_p$ and ω_c .

 J_0 is a cost phrase that refers to the closeness of static impediments. For example, in offpath conditions, an occupation grid cost-map C_0 based on perceptual data can be pre-determined at the start of every planning process. A cost function is applied to every grid-map cell. As a result, J_0 can be calculated by adding up the costs of the units occupied by the robotic body, as shown in (6), where $\tau_i (i = 1, ..., N)$ signifies a produced path. The divergence from the standard path is described by the cost term J_d . The divergence range of the produced path from the standard path is denoted by $D(\tau_i(s))$. We specify the smoothing criteria as J_s , that is achieved by incorporating the path curve, to increase the cleanliness of a produced path. In addition, the value term J_p is defined, which shows the preferences for longer viable routes. L_{max} Seems to be the maximum look-ahead length, and I seems to be the arc length is along referencing path, as shown in (6). The disparity of sequential designs during the preplanning stage can simply lead to overshoots, fluctuations, or even disturbances of robotic navigation. The mismatch among the present analyzed path, as well as the prior planned pathway, is taken into consideration to reduce inconsistencies. By incorporating the Euclidean distances $d(\tau_i(s))$ among them along the standard path, the value factor J_c is calculated. Optimizing criteria may be described as follows, taking into account all the above value factors:

$$N = \frac{N}{arg \min\{\omega_0 J_0(\tau_i) + \omega_d J_d(\tau_i) + \omega_s J_s(\tau_i) + \omega_p J_p(\tau_i) + \omega_c J_c(\tau_i)\}}{i = 1} = \frac{\{\omega_0 \int_0^{s_f} C_0(\tau_i(s)) ds + \omega_s J_s(\tau_i) + \omega_s J_s(\tau_i) + \omega_s J_s(\tau_i)\}}{\sum_{max} \int_0^{s_f} \frac{|D(\tau_i(s))|}{D_{max}} ds + \frac{\omega_s}{s_f} \int_0^{s_f} \frac{|D(\tau_i(s))|}{D_{max}} ds + \omega_p \frac{L_{max} - l(\tau_i)}{L_{max}} + \frac{\omega_c}{s_f} \int_0^{s_f} \frac{d(\tau_i(s))}{d_{max}} ds \}$$
(6)

The weighting factors can be adjusted easily as per navigating situations in reality. The ideal path is chosen among the pathway alternatives and monitored by the low-level controllers.

b. Iterative Learning Control Law:

A typical approach for robotic manipulator path monitoring control is the incremental learning control algorithms. It is vital to lower the number of repetitions needed for resolution while maintaining overall convergence of incremental learning control rule in addition to increase the manipulator's path monitoring speed. As a result, when designing an incremental learning control rule, both the original state error as well as the error's converging speed are taken into account.

The robotic manipulator (1) can be represented $asx_k(t) = [q \quad \dot{q}]^T$, as well as the movement and velocity of every manipulator's joints, are employed as its output signal:

$$\begin{cases} \dot{x}_{k} = \begin{bmatrix} \dot{q} \\ \ddot{q} \end{bmatrix} = f(x_{k}(t), t) + B(t)u_{k}(t) + W_{k}(t), \\ y_{k}(t) = C(t)x_{k}(t) + V_{k}(t), \end{cases}$$
(7)

where condition disruption and output disruption are $W_k(t)$ and $V_k(t)$, correspondingly. The quantity of repetitions is k.

$$f(x_k(t), t) = \begin{bmatrix} q \\ -M^{-1}(C(q, \dot{q})\dot{q} + G(q)) \end{bmatrix},$$

$$B(t) = \begin{bmatrix} 0 \\ M^{-1}(q) \end{bmatrix},$$

$$W_k(t) = \begin{bmatrix} 0 \\ -M^{-1}(q) \end{bmatrix} u_a,$$

$$C(t) = I.$$

(8)

The following requirements are expected to be met by the robotic manipulator system described above.

Assumption 1: The Lipschitz criterion is satisfied by $f(x_k(t), t)$; such that, there occurs a constant $L_f(L_f > 0)$ that meets the accompanying:

$$\|f(x_{k+1}(t),t) - f(x_k(t),t)\| \le L_f \|x_{k+1}(t) - x_k(t)\|.$$
(9)

Assumption 2: The output disruption variance and the neighboring state disruption variance are both limited, as follows:

$$\begin{cases} \|W_{k+1}(t) - W_k(t)\| \le b_w, \\ \|V_{k+1}(t) - V_k(t)\| \le b_V. \end{cases}$$
(10)

Assumption 3: B(t) and C(t) are both constrained.

Assumption 4: For every $t \in [0, T]$, the predicted path $y_d(t)$ is continual.

The mechanism is considered to have a randomized initial defect, represented by $e_k(t) = y_d(t) - y_k(t)$, as well as the *k*th iteration's basic value is $x_k(0)$. The following is the control law:

$$v_k(t) = v_{k-1}(t) + \Gamma e_k(t) + \Gamma \dot{e_k}(t) + \phi_k(t) X_k(0), \quad t \in [0, T],$$
(11)

while Γ is the uniform gain matrix also $G_c = \Gamma(e_k(t) + \dot{e_k}(t) + \phi_k(t)X_k(0))$.

The beginning state's learning rule is

$$\emptyset(t) = \begin{cases} \frac{2a^{k}}{h} \left(1 - \frac{a^{k}}{h}t\right), & t \in \left[0, \frac{h}{a^{k}}\right], \\ 0, & t \in \left[\frac{h}{a^{k}}, T\right], \\ a > 1, 0 < h < T, \end{cases}$$

$$X_{k}(0) = B(0) \Gamma e_{k}(0) + x_{k}(0) - x_{k+1}(0), \qquad (13)$$

here a > 1, 0 < h < T.

The original state defect only can impact the path monitoring speed within the period $[0, (\frac{h}{a^k})]$, according to equation (12). The original state defect will also be 0 after $t = h/a^k$. The timing moment h/a^k will rapidly decrease to zero because as the number of repetitions k increases, implying that the duration of the original state mistake affects the path monitoring speed will also be relatively short. It implies that by employing the suggested incremental learning control rule, the path monitoring speed can also be enhanced.

PERFORMANCE ANALYSIS

We perform experiments on such a simulated scenario to verify the efficiency of the suggested strategy. The robot's beginning speed is fixed to 60 km/h, with a maximum speed of 100 km/h. The maximum precise values of lateral and longitudinal velocity are set at 3 and 5 meters per second, correspondingly. Path planning as well as low-level monitoring controls cycle times are fixed to 100ms and 20ms, correspondingly. The maximum look-ahead range has been set at 50 meters. A first-order delaying method is used to describe the reaction of low-level controllers.

The robotics' whole monitoring results along a standard path with two boundaries. When traveling at a fast speed, the robot is proficient in evading static obstructions while remaining in the path. The robot's horizontal navigation inaccuracy is depicted in Figure 4. The horizontal monitoring defects are less than 1m over the whole track, as can be observed. The transverse is modified as per the standard pathway geometry, in addition, to ensure security and convenience while keeping speeding limitations in various path sections, as seen in Fig. 11.



Figure 4: Horizontal navigation of robot.



Figure 5: Robot speed conditions.

CONCLUSION

By merging regional path planning and monitoring control in such a unified architecture, this research proposes a regional guidance approach for autonomous robots moving along a referral route. As in the

path planning step, we propose a sampling-based path planner that follows a discontinuous optimization strategy, in addition, to seamlessly track the standard path and respond to unexpectedly altering circumstances, and also increase navigating safety and convenience. The planner takes into account its geometry of standard pathway, static barrier minimization, robotic kinematics, and certain dynamic restrictions to assure that the planned path is dynamically feasible. During the low-level monitoring control step, the guiding instructions are generated using the robotic steady-state guiding features, which are then utilized to follow the required yaw values obtained from the determined optimum path.

The simulated findings show that the suggested unified regional path planning with a monitoring control structure is capable of following a standard track while eliminating static barriers at such a great speed. We will continue to research expanding the suggested structure in the future. In congested situations, for example, one prospective enhancement is to combine the local route optimization technique with graph-search path planners and construct dynamically feasible paths in continual space rather than discontinuous search space.

REFERENCE

- 1. J. Levinson, et al., "Towards fully autonomous driving: systems and algorithms," IEEE Intell. Veh. Symp., pp. 163–168, 2011.
- 2. J. B. Derrick and D. M. Bevly, "Adaptive steering control of a farm tractor with varying yaw rate properties," J. Field Robotics, vol. 26, no. 6–7, pp. 519–536, 2009.
- 3. X. Min and M. A. Minor, "Variable structure backstepping control via a hierarchical manifold set for graceful ground vehicle path following," IEEE Int. Conf. on Robotics and Auto., pp. 2826–2832, 2013.
- 4. J. M. Snider, "Automatic steering methods for autonomous automobiles," Tech. Rep. CMU-RI-TR-09-08, Robotics Institute, Pittsburgh, PA. Feb. 2009.
- 5. P. Falcone, et al., "Predictive active steering control for autonomous vehicle systems," IEEE Trans. Control Syst. Technol., vol. 15, no. 3, pp. 566–580, 2007.
- 6. S. J. Anderson, et al., "An optimal-control-based framework for trajectory planning, threat assessment, and semi-autonomous control of passenger vehicles in hazard avoidance scenarios," Int. J. Vehicle Autonomous Systems, vol. 18, no. 2–4, pp. 190–215, 2010.
- 7. C. E. Beal and J. C. Gerdes, "Model predictive control for vehicle stabilization at the limits of handling," IEEE Trans. on Control Systems Technology, vol. 21, no. 4, pp. 1258–1269, 2013.
- L. Pan, T. Gao, F. Xu, and L. Zhang, "Enhanced robust motion tracking control for 6 degree-offreedom industrial assembly robot with disturbance adaption," International Journal of Control, Automation and Systems, vol. 16, no. 2, pp. 921–928, 2018.
- 9. J. Li, Y. Zhang, and M. Mao, "Continuous and discrete zeroing neural network for different-level dynamic linear system withrobot manipulator control," IEEE Transactions on Systems, Man, and Cybernetics: Systems, pp. 1–10, 2018.
- Y. Wang, L. Gu, Y. Xu, and X. Cao, "Practical tracking control of robot manipulators with continuous fractional-order non-singular terminal sliding mode," IEEE Transactions on Industrial Electronics, vol. 63, no. 10, pp. 6194–6204, 2016.

- Dumlu and K. Erenturk, "Trajectory tracking control for a 3-DOF parallel manipulator using fractional-order PIλ Dµ control," IEEE Transactions on Industrial Electronics, vol. 61, no. 7, pp. 3417–3426, 2014.
- Izadbakhsh and S. Khorashadizadeh, "Robust task-space control of robot manipulators using differential equations for uncertainty estimation," Robotica, vol. 35, no. 9, pp. 1923–1938, 2017.
- R. S. Mohammad, H. Jafaar, and S. Mahmoodreza, "Robust nonlinear control of robot manipulator with uncertainties in Kinematics, Dynamics and actuator models," International Journal of Innovative Computing, Information and Control, vol. 8, no. 8, pp. 5487–5489, 2012.
- 14. Andreev and O. Peregudova, "Trajectory tracking control for robot manipulators using only position measurements," International Journal of Control, vol. 92, no. 7, pp. 1490–1496, 2017.
- 15. P. Farzin, M. Mina, S. Forouzan, N. Iman, and E. Sara, "Design baseline computed torque controller," International Journal of Engineering (IJE), vol. 6, no. 3, pp. 129–141, 2012.
- Suresh, P., Rajesh, K.B. and Sivasubramonia Pillai, T.V. and Jaroszewicz, Z., "Effect of annular obstruction and numerical aperture in the focal region of high NA objective lens," Elsevier – Optics Communication, Vol – 318, 2014, pp. 137–141.
- H. Reham, F. Bendary, and K. Elserafi, "Trajectory tracking control for robot manipulator using fractional order-fuzzyPID controller," International Journal of Computer Applications, vol. 134, no. 15, pp. 22–29, 2016.
- 18. T. Ye, Z. Luo, and G. Wang, "Adaptive sliding mode control of robot based on fuzzy neural network," Journal of Ambient Intelligence and Humanized Computing, 2020.
- 19. T. M. Howard, et al., "State space sampling of feasible motions for high-performance mobile robot navigation in complex environments," J. Field Robotics, vol. 25, no. 6–7, pp. 325–345, 2008.
- 20. F. V. Hundelshausen, et al., "Driving with tentacles: integral structures for sensing and motion,"J. Field Robotics, vol. 25, no. 9, pp. 640–673, 2008.
- 21. Broggi, et al., "Autonomous vehicles control in the VisLab inter-continental autonomous challenge," Annu. Rev. control, vol. 36, no. 1, pp. 161–171, 2012.
- 22. Suresh, P., Thilagavathi. R., Gokulakrishnan, K., Rajesh, K.B. and Pillai, T.V.S., "Focusing properties of a 4Pi configuration system under the illumination of double ring shaped LG11 beam," Springer Optical and Quantum Electronics, 1-6, 2014
- 23. Kelly and T. Stenz, "Rough terrain autonomous mobility part2: An active vision and prediction control approach," Autonomous Robots, vol. 5, pp. 163–198, 1998.
- 24. E. Frazzoli, M. A. Dahleh and E. Feron, "Real-time motion planning for agile autonomous vehicles," J. Guid. Control Dynam., vol. 25, no. 1, pp. 116–129, 2002.
- 25. K. Yang and S. Sukkarieh, "An analytical continuous-curvature path-smoothing algorithm," IEEE Trans. on Robotics, vol. 26, no. 3, pp. 561–568, 2010.
- 26. S. Thrun, et al., "Stanley: The robot that won the DARPA grand challenge," J. Field Robotics, vol. 23, no. 9, pp. 661-692, 2006.
- 27. U. Schwesinger, et al., "A sampling-based partial motion planning framework for systemcompliant navigation along a reference path," IEEE Intell. Veh. Symp., pp. 391–396, 2013.

- 28. Y. Kuwata, et al., "Real-time motion planning with applications to autonomous urban driving," IEEE Trans. Control Syst. Technol., vol. 17, no. 5, pp. 1105–1118, 2009.
- 29. T. Howard and A. Kelly, "Optimal rough terrain trajectory generation for wheeled mobile robots," Int. J. Robot. Res., vol. 26, no. 2, pp. 141–166, 2007.
- 30. Hewit JR and Burdess JS. Fast dynamic decoupled control for robotics using active force control. Trans Mech Mach Theory 1981; 16(5): 535–542.
- 31. Hewit JR and Marouf KB. Practical control enhancement via mechatronics design. IEEE Trans Ind Electron 1996; 43(1): 16–22.
- 32. Mailah M.Intelligent active force control of a rigid robot arm using neural network and iterative learning algorithms. PhD Thesis, University of Dundee, UK, 1998.
- 33. Kwek LC, Wong EK, Loo CK, et al. Application of active force control and iterative learning in a 5link biped robot. J Intell Robot Syst 2003; 37: 143–162.
- 34. Luh JYS, Walker MW and Paul RPC. Resolved acceleration control of mechanical manipulator. IEEE Trans Automat Contr 1980; 25: 486–474.
- Suresh, P., Mariyal, C., Gokulakrishnan, K., Rajesh, K.B. and Pillai, T.V.S., "Tight Focusing of Circularly Polarized Beam over high NA Lens Axicon with a Diffractive Optical Element," Elsevier – Optik, vol. 124. Issue 20, 2013. pp. 4389-4392
- 36. Tang HH, Mailah M and Jalil MKA, Robust intelligent active force control of non-holonomic wheeled mobile robot. J Teknologi 2006; 44(D): 4964.
- 37. Chao C, Chengrui Z, Tianliang H, et al. Model-assisted extended state observer-based computed torque control for trajectory tracking of uncertain robotic manipulator systems. Int J Adv Robot Syst 2018; 15(5): 1–12.
- 38. Boukattaya M, Mezghani N and Damak T. Computed-torque control of a wheeled mobile manipulator. Int J Robot Eng 2018; 3(5): 1–6.
- 39. Mohammed AHA. Autonomous mobile robot navigation and control in the road following and roundabout environments are incorporating laser range finder and vision system. PhD Thesis, Universiti Teknologi Malaysia, Malaysia, 2014.